

CPC COOPERATIVE PATENT CLASSIFICATION

H03D DEMODULATION OR TRANSFERENCE OF MODULATION FROM ONE CARRIER TO ANOTHER (masers, lasers [H01S](#); circuits capable of acting both as modulator and demodulator [H03C](#); details applicable to both modulators and frequency-changers [H03C](#); demodulating pulses [H03K 9/00](#); transforming types of pulse modulation [H03K 11/00](#); coding, decoding or code conversion, in general [H03M](#); repeater stations [H04B 7/14](#); demodulators adapted for ac systems of digital information transmission [H04L 27/00](#); synchronous demodulators adapted for colour television [H04N 9/66](#))

NOTE

This subclass covers only:

- demodulation or transference of signals modulated on a sinusoidal carrier or on electromagnetic waves;
- comparing phase or frequency of two mutually-independent oscillations.

1/00	Demodulation of amplitude-modulated oscillations (H03D 5/00 , H03D 9/00 , H03D 11/00 take precedence)	1/26	• by means of transit-time tubes
1/02	• Details	1/28	• by deflecting an electron beam in a discharge tube (H03D 1/26 takes precedence)
1/04	• . Modifications of demodulators to reduce interference by undesired signals	3/00	Demodulation of angle-, {frequency- or phase-} modulated oscillations (H03D 5/00 , H03D 9/00 , H03D 11/00 take precedence)
1/06	• . Modifications of demodulators to reduce distortion, e.g. by negative feedback	3/001	• {Details of arrangements applicable to more than one type of frequency demodulator (H03D 3/28 takes precedence)}
1/08	• by means of non-linear two-pole elements (H03D 1/22 , H03D 1/26 , H03D 1/28 take precedence)	3/002	• . {Modifications of demodulators to reduce interference by undesired signals (H03D 3/248 takes precedence)}
1/10	• . of diodes	3/003	• . {Arrangements for reducing frequency deviation, e.g. by negative frequency feedback (combined with a phase locked loop demodulator H03D 3/242 ; changing frequency deviation for modulators H03C 3/06)}
1/12	• . . with provision for equalising ac and dc loads	3/004	• . . {wherein the demodulated signal is used for controlling an oscillator, e.g. the local oscillator}
1/14	• by means of non-linear elements having more than two poles (H03D 1/22 , H03D 1/26 , H03D 1/28 take precedence)	3/005	• . . {wherein the demodulated signal is used for controlling a bandpass filter (automatic bandwidth control H03G ; automatic frequency control H03J 7/02)}
1/16	• . of discharge tubes	3/006	• {by sampling the oscillations and further processing the samples, e.g. by computing techniques (H03D 3/007 takes precedence)}
1/18	• . of semiconductor devices	3/007	• {by converting the oscillations into two quadrature related signals (H03D 3/245 takes precedence)}
1/20	• . with provision for preventing undesired type of demodulation, e.g. preventing anode detection in a grid detection circuit	3/008	• . {Compensating DC offsets}
1/22	• Homodyne or synchrodyne circuits {(receiver circuits H04B 1/30)}	3/009	• . {Compensating quadrature phase or amplitude imbalances}
1/2209	• . {Decoders for simultaneous demodulation and decoding of signals composed of a sum-signal and a suppressed carrier, amplitude modulated by a difference signal, e.g. stereocoders}	3/02	• by detecting phase difference between two signals obtained from input signal (H03D 3/28 - H03D 3/32 take precedence; {muting in frequency-modulation receivers H03G 3/28 }; limiting arrangements H03G 11/00)
1/2218	• . . {using diodes for the decoding}	3/04	• . by counting or integrating cycles of oscillations {(arrangements for measuring frequencies G01R 23/10)}
1/2227	• . . {using switches for the decoding (diodes used as switches H03D 1/2218)}	3/06	• . by combining signals additively or in product demodulators
1/2236	• . . {using a phase locked loop}	3/08	• . . by means of diodes, e.g. Foster-Seeley discriminator
1/2245	• . {using two quadrature channels (H03D 1/2209 takes precedence)}		
1/2254	• . . {and a phase locked loop}		
2001/2263	• . . . {including a counter or a divider in the PLL}		
1/2272	• . {using FET's (H03D 1/2209 , H03D 1/2245 and H03D 1/2281 take precedence)}		
1/2281	• . {using a phase locked loop (H03D 1/2236 and H03D 1/2254 take precedence)}		
1/229	• . {using at least a two emitter-coupled differential pair of transistors (H03D 1/2209 - H03D 1/2281 take precedence)}		
1/24	• . for demodulation of signals wherein one sideband or the carrier has been wholly or partially suppressed {(receiver circuits H04B 1/302)}		

- 3/10 . . . in which the diodes are simultaneously conducting during the same half period of the signal, e.g. radio detector
- 3/12 . . . by means of discharge tubes having more than two electrodes
- 3/14 . . . by means of semiconductor devices having more than two electrodes
- 3/16 . . . by means of electromechanical resonators
- 3/18 . . by means of synchronous gating arrangements
- 3/20 . . . producing pulses whose amplitude or duration depends on phase difference
- 3/22 . . by means of active elements with more than two electrodes to which two signals are applied derived from the signal to be demodulated and having a phase difference related to the frequency deviation, e.g. phase detector
- 3/24 . . Modifications of demodulators to reject or remove amplitude variations by means of locked-in oscillator circuits
- 3/241 . . . {the oscillator being part of a phase locked loop}
- 3/242 {combined with means for controlling the frequency of a further oscillator, e.g. for negative frequency feedback or AFC}
- 3/244 {combined with means for obtaining automatic gain control}
- 3/245 {using at least twophase detectors in the loop ([H03D 3/244 takes precedence](#); in general [H03L 7/087](#))}
- 3/247 {using a controlled phase shifter (in general [H03L 7/081](#))}
- 3/248 {with means for eliminating interfering signals, e.g. by multiple phase locked loops (multiple loops in general [H03L 7/07](#), [H03L 7/22](#))}
- 3/26 . . by means of sloping amplitude/frequency characteristic of tuned or reactive circuit ([H03D 3/28 - H03D 3/32 takes precedence](#))
- 3/28 . . Modifications of demodulators to reduce effects of temperature variations ({[automatic frequency regulation in receivers H03J](#)}; automatic frequency control [H03L](#))
- 3/30 . . by means of transit-time tubes
- 3/32 . . by deflecting an electron beam in a discharge tube ([H03D 3/30 takes precedence](#))
- 3/34 . . by means of electromechanical devices ([H03D 3/16 takes precedence](#))
- 5/00** **Circuits for demodulating amplitude-modulated or angle-modulated oscillations at will ([H03D 9/00](#), [H03D 11/00](#) take precedence)**
- 7/00** **Transference of modulation from one carrier to another, e.g. frequency-changing ([H03D 9/00](#), [H03D 11/00](#) take precedence; dielectric amplifiers, magnetic amplifiers, parametric amplifiers used as a frequency-changers [H03F](#))**
 - 7/005 . . {by means of superconductive devices}
 - 7/02 . . by means of diodes ([H03D 7/14 - H03D 7/22 take precedence](#))
 - 7/04 . . having {a partially} negative resistance characteristic, e.g. tunnel diode
 - 7/06 . . by means of discharge tubes having more than two electrodes ([H03D 7/14 - H03D 7/22 take precedence](#))
- 7/08 . . the signals to be mixed being applied between the same two electrodes
- 7/10 . . the signals to be mixed being applied between different pairs of electrodes
- 7/12 . . by means of semiconductor devices having more than two electrodes ([H03D 7/14 - H03D 7/22 take precedence](#))
- 7/125 . . {with field effect transistors}
- 7/14 . . Balanced arrangements
- 7/1408 . . {with diodes}
- 7/1416 . . {with discharge tubes having more than two electrodes}
- 7/1425 . . {with transistors}
- WARNING**
Subgroups [H03D 7/1433 - H03D 7/1491](#) are incomplete pending reclassification; see also this group and its other subgroups
- 7/1433 . . . {using bipolar transistors ([H03D 7/145 takes precedence](#))}
- 7/1441 . . . {using field-effect transistors ([H03D 7/145 takes precedence](#))}
- 7/145 . . . {using a combination of bipolar transistors and field-effect transistors}
- 7/1458 . . . {Double balanced arrangements, i.e. where both input signals are differential}
- 7/1466 . . . {Passive mixer arrangements}
- 7/1475 . . . {Subharmonic mixer arrangements}
- 7/1483 . . . {comprising components for selecting a particular frequency component of the output}
- 7/1491 . . . {Arrangements to linearise a transconductance stage of a mixer arrangement}
- 7/16 . . Multiple-frequency-changing
- 7/161 . . {all the frequency changers being connected in cascade}
- 7/163 . . . {the local oscillations of at least two of the frequency changers being derived from a single oscillator}
- 7/165 . . {at least two frequency changers being located in different paths, e.g. in two paths with carriers in quadrature (combined with amplitude demodulation [H03D 1/2245](#), combined with angle demodulation [H03D 3/007](#); N-path filters [H03H 19/002](#))}
- 7/166 . . . {using two or more quadrature frequency translation stages}
- 7/168 {using a feedback loop containing mixers or demodulators}
- 7/18 . . Modifications of frequency-changers for eliminating image frequencies ({[H03D 7/16 takes precedence](#))}
- 7/20 . . by means of transit-time tubes
- 7/22 . . by deflecting an electron beam in a discharge tube ([H03D 7/20 takes precedence](#))
- 9/00** **Demodulation or transference of modulation of modulated electromagnetic waves (demodulating light, transferring modulation in light waves [G02F 2/00](#))**
 - 9/02 . . Demodulation using distributed inductance and capacitance, e.g. in feeder lines
 - 9/04 . . for angle-modulated oscillations
 - 9/06 . . Transference of modulation using distributed inductance and capacitance
 - 9/0608 . . {by means of diodes}

9/0616	. . . {mounted in a hollow waveguide (H03D 9/0641 takes precedence)}	2200/0019	. . Gilbert multipliers
9/0625	. . . {mounted in a coaxial resonator structure}	2200/0021	. . Frequency multipliers
9/0633	. . . {mounted on a stripline circuit}	2200/0023	. . Balun circuits
9/0641 {located in a hollow waveguide}	2200/0025	. . Gain control circuits
9/065	. . {by means of discharge tubes having more than two electrodes}	2200/0027	. . . including arrangements for assuring the same gain in two paths
9/0658	. . {by means of semiconductor devices having more than two electrodes}	2200/0029	. . Loop circuits with controlled phase shift
9/0666	. . . {using bipolar transistors (H03D 9/0683 takes precedence)}	2200/0031	. . PLL circuits with quadrature locking, e.g. a Costas loop
9/0675	. . . {using field effect transistors (H03D 9/0683 takes precedence)}	2200/0033	. . Current mirrors
9/0683	. . . {using a combination of bipolar transistors and field effect transistors}	2200/0035	. . Digital multipliers and adders used for detection
2009/0691	. . {by means of superconductive devices}	2200/0037	. . Diplexers
11/00	Super-regenerative demodulator circuits {(applications in responders G01S)}	2200/0039	. . Exclusive OR logic circuits
11/02	. for amplitude-modulated oscillations	2200/0041	. Functional aspects of demodulators
11/04	. . by means of semiconductor devices having more than two electrodes	2200/0043	. . Bias and operating point
11/06	. for angle-modulated oscillations	2200/0045	. . Calibration of demodulators
11/08	. . by means of semiconductor devices having more than two electrodes	2200/0047	. . Offset of DC voltage or frequency
13/00	Circuits for comparing the phase or frequency of two mutually-independent oscillations {(measuring phase G01R 25/00; phase-discriminators with yes/no output G01R 25/005)}	2200/0049	. . Analog multiplication for detection
13/001	. {in which a pulse counter is used followed by a conversion into an analog signal}	2200/005	. . Analog to digital conversion
13/002	. . {the counter being an up-down counter}	2200/0052	. . Digital to analog conversion
13/003	. {in which both oscillations are converted by logic means into pulses which are applied to filtering or integrating means}	2200/0054	. . Digital filters
13/004	. . {the logic means delivering pulses at more than one terminal, e.g. up and down pulses}	2200/0056	. . . including a digital decimation filter
13/005	. {in which one of the oscillations is, or is converted into, a signal having a special waveform, e.g. triangular}	2200/0058	. . . using a digital filter with interpolation
13/006	. . {and by sampling this signal by narrow pulses obtained from the second oscillation}	2200/006	. . Signal sampling
13/007	. {by analog multiplication of the oscillations or by performing a similar analog operation on the oscillations}	2200/0062	. . . Computation of input samples, e.g. successive samples
13/008	. . {using transistors}	2200/0064	. . Detection of passages through null of a signal
13/009	. . {using diodes}	2200/0066	. . Mixing
99/00	Subject matter not provided for in other groups of this subclass	2200/0068	. . . by computation
2200/00	Indexing scheme relating to details of demodulation or transference of modulation from one carrier to another covered by H03D	2200/007	. . . by using a logic circuit, e.g. flipflop, XOR
2200/0001	. Circuit elements of demodulators	2200/0072	. . . by complex multiplication
2200/0003	. . Rat race couplers	2200/0074	. . . using a resistive mixer or a passive mixer
2200/0005	. . Wilkinson power dividers or combiners	2200/0076	. . . using a distributed mixer
2200/0007	. . Dual gate field effect transistors	2200/0078	. . . using a switched phase shifter or delay line
2200/0009	. . Emitter or source coupled transistor pairs or long tail pairs	2200/008	. . Hilbert type transformation
2200/0011	. . Diodes	2200/0082	. . Quadrature arrangements
2200/0013	. . . Diodes connected in a ring configuration	2200/0084	. . Lowering the supply voltage and saving power
2200/0015	. . . Diodes connected in a star configuration	2200/0086	. . Reduction or prevention of harmonic frequencies
2200/0017	. . Intermediate frequency filter	2200/0088	. . Reduction of intermodulation, nonlinearities, adjacent channel interference; intercept points of harmonics or intermodulation products
		2200/009	. . Reduction of local oscillator or RF leakage
		2200/0092	. . Detection or reduction of fading in multipath transmission arrangements
		2200/0094	. . Measures to address temperature induced variations of demodulation
		2200/0096	. . . by stabilising the temperature
		2200/0098	. . . by compensating temperature induced variations